

# The Effect of Reinforcement Amount and Sintering Temperature on Mg Matrix Composite Fabricated by Powder Metallurgy

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**ABSTRACT.** A metal matrix composite (MMC) is known as high tech composites and useful and magnesium (Mg) is among the suitable metal for producing composites. Combining Mg, Zinc (Zn) and Alumina ( $Al_2O_3$ ) powders will yield a composite with improved corrosive resistance, mechanical properties and abrasive wear behavior. So, the aim of this research is to study the effect of reinforcement ( $Al_2O_3$ ) and sintering temperature (300 °C and 550 °C) on Mg-Zn alloy matrix composite fabricated by powder metallurgy. The powder mixture of pure Mg, Mg-Zn alloy and Mg-Zn/15%  $Al_2O_3$  composite was milled separately in a planetary mill under gas argon atmosphere using a stainless steel container and balls. Milling process was carried out at 220 rpm for 2 hours and 3% of n-heptane solution was added prior to milling process to avoid the excessive cold welding of the powder. The powder was compacted under 400MPa and sintered with different sintering temperature with 300 °C and 550 °C in a tube furnace for 1hour under the flow of argon. The density of the sintered pellets was then determined by Archimedes principle. Mechanical properties of the sintered pellets were characterized by microhardness and compressive test. The results shows that the density, hardness and compressive strength of Mg-Zn/15%  $Al_2O_3$  composite was higher compared to pure Mg and Mg-Zn alloy at temperature 300 °C compared to 550 °C.

**Keywords:** Metal matrix composites, Zinc, Alumina, Powder metallurgy;

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## 1. INTRODUCTION

In order to limit the fuel consumption and carbon dioxide emission, the structural weight of the vehicles need to be reduced [1]. Mg as the lightest metallic structural material, low density, excellent damping capacity and good machinability [2,3] becomes potential candidates for a variety in engineering application. However, the limitations of Mg which include poor elastic modulus and high temperature strength properties [4] restrict its utilization in critical engineering application [3-6]. In order to minimize these limitations, Mg metal matrix being developed with reinforced Mg with Zn and  $Al_2O_3$ . In the past, to manufacture MMC, ceramic reinforcing phases such as oxides ( $Al_2O_3$ ,  $SiO_2$ ), carbides ( $SiC$ ,  $B_4C$ ) and nitrides ( $Si_3N_4$ ) were used in order to optimize their structure and properties [6].

Powder metallurgy (PM) is one of the best methods in preparation of MMC [7]. The main advantages of PM are relatively low processing temperature, provide great freedom degree in tailoring the microstructure such as volume fraction and morphology, where better distribution of the reinforcement is possible in PM compacts [8]. It also approved by experiment and theoretical studies. For composite fabricated by the powder metallurgy method, it is possible when the matrix to reinforcement particle size ratio is close to unity [9]. With increasing metal working characteristics, particulate reinforced MMCs improved both mechanical and physical properties. Besides that, powder metallurgy processing is one of the methods for fabricating these

materials [10]. MMCs are important because of their high Young modulus, high abrasive properties and high ratio of strength and weight [11]. The present study aims to investigate the effect of Zn and Al<sub>2</sub>O<sub>3</sub> content on Mg and to study the effect of sintering temperature on the density, relative density, hardness and compressive strength of Mg.

## 2. MATERIALS AND METHODS

A mixture of elemental Mg powder (99.0% pure), Zn powder (99.0% pure) and Al<sub>2</sub>O<sub>3</sub> (99.0% pure) corresponding to Mg-Zn was mechanically milled. Proper proportional of the powders were placed in a planetary ball mill for 2 hours and 220 rpm using high-energy Fritsch Pulverisste P-5 planetary mill under argon atmosphere. 3% of n-heptane solution was used as a process control agent to prevent excessive cold welding of the elemental alloy powders. A number of 20 mm diameter stainless steel balls were loaded together with all the powders in a 250 ml stainless steel vial and the vial was sealed with rubber O-ring. Ball to powder ratio was 1:8.75 was kept constant during the milling process. Conventional powder metallurgy (uniaxial pressing) was employed to produce the samples. Green compacts were cold pressed under 400 MPa and were sintered in argon at 300 °C and 550 °C for 1 hour. Density measurements were done using pycnometer density equipment according to Archimedes's principles. Vickers microhardness test was carried out by applying an indentation load of 300 gf for 10 s. Compression test were done using machine instron 5982 with diameter 10 mm and length of 10 mm.

## 3. RESULTS AND DISCUSSION

Fig. 1 portrayed the sintered density of the pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composite that was sintered with different sintering temperature of 300 °C and 550 °C. The sintered density was found to increase as two particles Zn and Al<sub>2</sub>O<sub>3</sub> were added into Mg. The sintered density for Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composites increased as compared to pure Mg and Mg-Zn alloy. The sintering temperature at 300 °C shows higher sintered density as compared to 550 °C in pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composites. The addition of 15% Al<sub>2</sub>O<sub>3</sub> increased the sintered density as compared to pure Mg and Mg-Zn alloy. This is due to the fact that the density of alumina is higher than that of magnesium. However this phenomenon is not comparative to the amount of alumina since alumina additions leads to the formation of pores. The density of Al<sub>2</sub>O<sub>3</sub> is 3.97 g/cm<sup>3</sup> while the density of pure Mg is 1.736 g/cm<sup>3</sup>. So, the sintered density with addition of alumina gave affect to the result of sintered density compared to pure Mg and Mg-Zn alloy.

Fig. 2 displayed the relative density of pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composite. Relative density of Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composite showed lowered compared to pure Mg and Mg-Zn alloy. Five readings were taken for each run and the average density was reported. The relative density (pr) was calculated by;

$$\rho_r = \rho_{ac} / \rho_{th} \times 100 \% \quad (1)$$

$$\rho_{th} = \rho_{Mg} V_{Mg} + \rho_{Zn} V_{Zn} + \rho_{HA} V_{HA} + \rho_{Al2O3} V_{Al2O3} \quad (2)$$

$$V_{Mg} + V_{Zn} + V_{HA} + V_{Al2O3} = 1 \quad (3)$$

Where  $\rho_r$ ,  $\rho_{ac}$  and  $\rho_{th}$  represent the relative density, actual density and theoretical density of the samples, respectively;  $\rho_{Mg} = 1.74 \text{ g/cm}^3$ ,  $\rho_{Zn} = 7.14 \text{ g/cm}^3$ ,  $\rho_{HA} = 3.16 \text{ g/cm}^3$  and  $\rho_{Al2O3} 3.97 \text{ g/cm}^3$ . The addition of alumina reduced the relative density in 300 °C compare to 550 °C. This may be due to the reduction in compressibility of the powder during sintering process. Besides that, this may be due to inhibiting effect of alumina in the rearrangement of the particles during sintering process. Furthermore, the melting points of the matrix and the reinforcement also give effects to the relative density. The melting point of alumina is 2072 °C and at higher sintering temperature 550 °C, the activation energy required for sintering mechanism to proceed neck growth and gave result to the surface and volume diffusion.

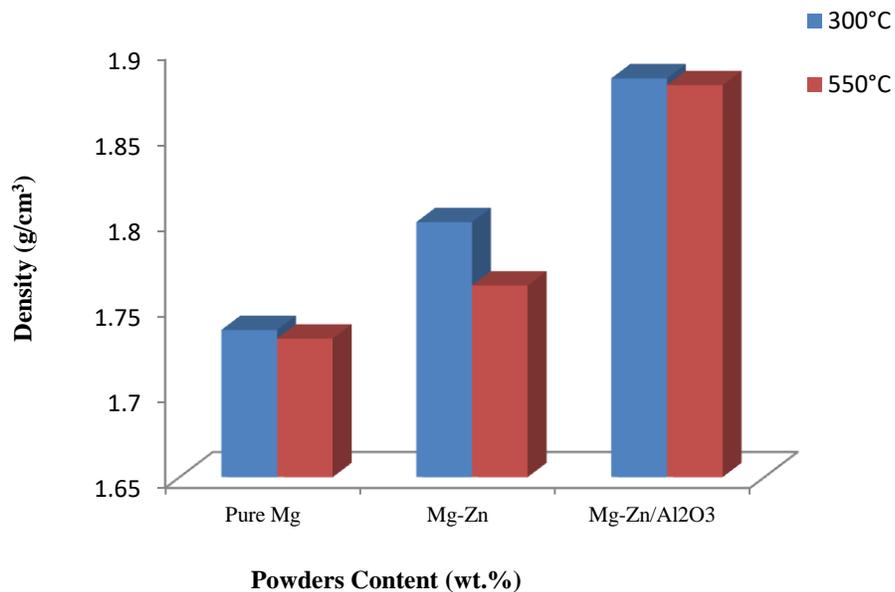


Fig. 1 Sintered density of pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composite

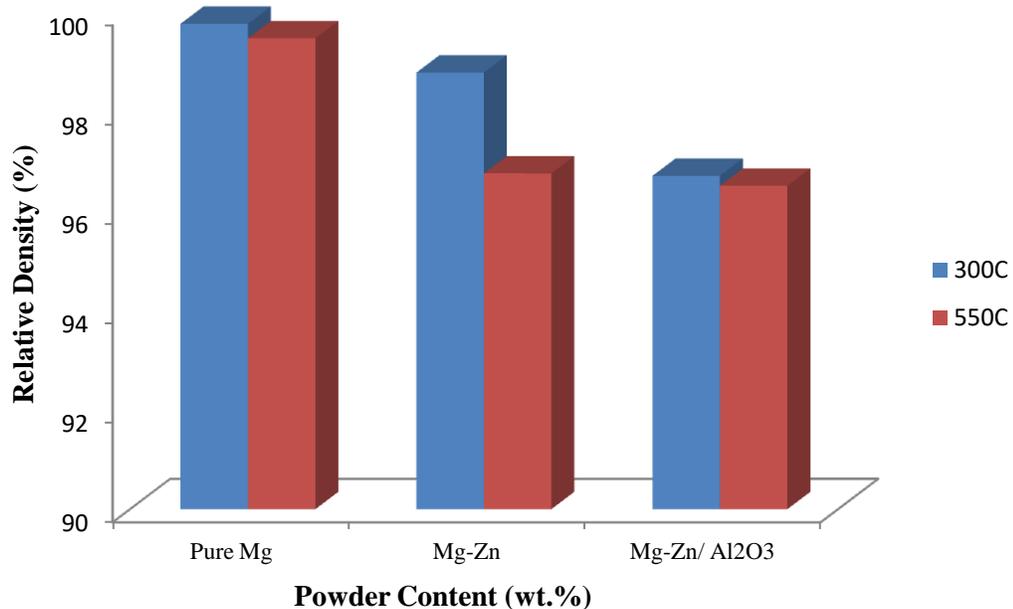
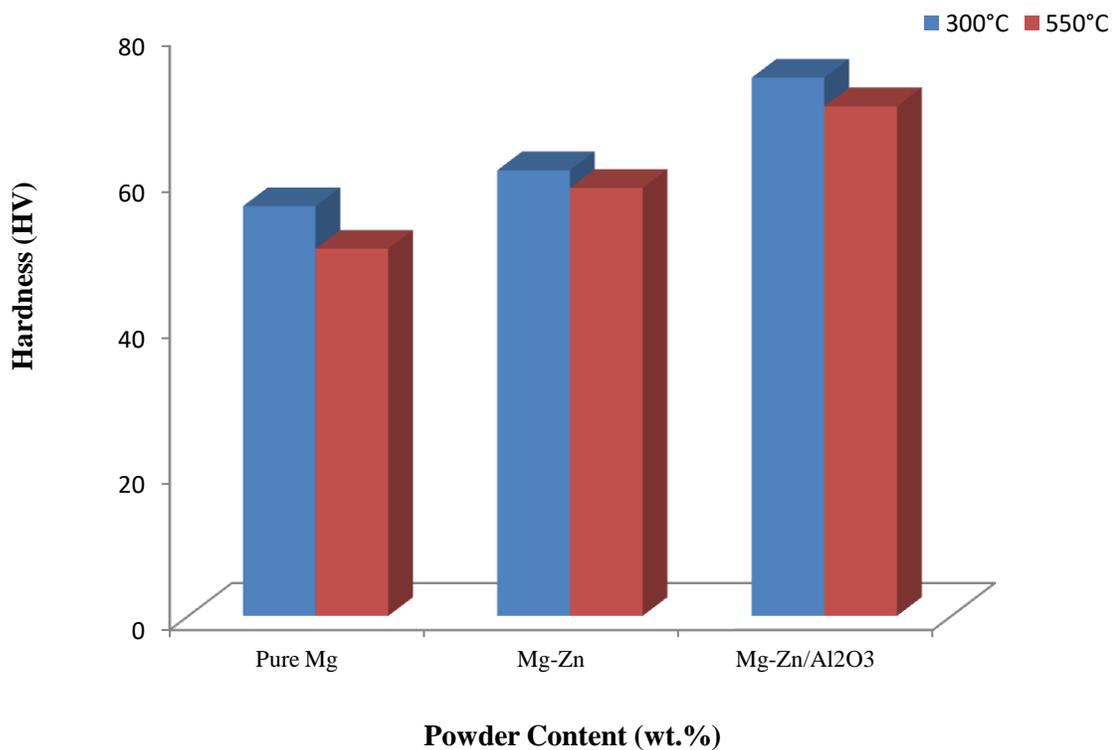


Fig.2 Relative density of pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composite.

The microhardness results of pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composites are shown in Fig. 3. It can be noticed that adding of 15% Al<sub>2</sub>O<sub>3</sub> particles into alloy matrix increased the hardness value. This can be attributed to the presence of harder reinforcements which offer high constraints during indentation. The microhardness of Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composites revealed higher hardness values as compared to pure Mg and

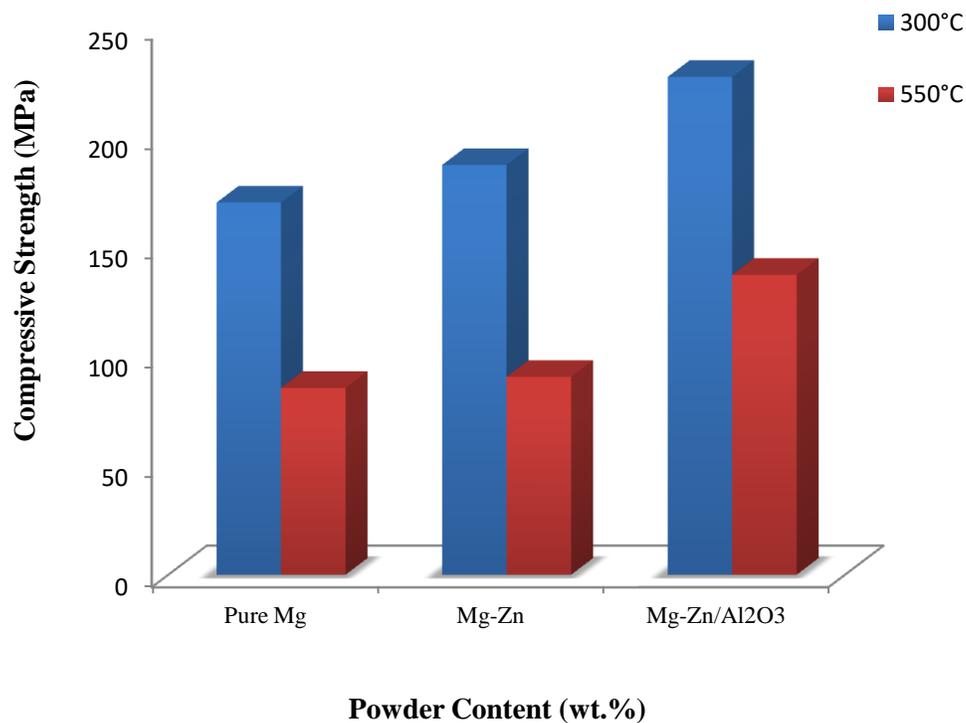
Mg-Zn alloys at different sintering temperature of 300 °C and 550 °C. An  $\text{Al}_2\text{O}_3$  particle acts as a barrier to the rearrangement, deformation and diffusion of the particles [12].

The harder  $\text{Al}_2\text{O}_3$  particles provide sufficient strength to the soft matrices and hence the microhardness values increases due to the dispersion strengthening effect. With gradual increases on  $\text{Al}_2\text{O}_3$  content the microhardness values increases as a result of uniform dispersion of the reinforcement within the matrices. The peak value of hardness was achieved with 15 wt.%  $\text{Al}_2\text{O}_3$  compare to pure Mg and Mg-Zn alloy. This mainly due to uniform dispersion of  $\text{Al}_2\text{O}_3$  and acts as hard particles that hinders the mobility of the defects (dislocations) in the matrix.



**Fig.3** Microhardness of pure Mg, Mg-Zn alloy and Mg-Zn/ $\text{Al}_2\text{O}_3$  composite

The results of compressive strength have been presented in Fig. 4. Ultimate compressive strength of the Mg-Zn/15%  $\text{Al}_2\text{O}_3$  composite appeared to have an increment in the compressive strength at sintering temperature 300 °C compare to 550 °C. It shows that sintering temperature gave effect to the result of compressive strength. The addition of  $\text{Al}_2\text{O}_3$  to Mg-Zn alloy increased the strength by a dispersion hardening mechanism.  $\text{Al}_2\text{O}_3$  particles being hard and brittle lead to dispersion hardening of matrix. These particles act as second phase in the matrix and resist the movement of dislocations and hence harden the composites [13].



**Fig.4** Compression test for Pure Mg, Mg-Zn alloy and Mg-Zn/Al<sub>2</sub>O<sub>3</sub> composites

#### 4. SUMMARY

In this study, pure Mg, Mg-Zn alloy and Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> composites were synthesized through powder metallurgy method. Superior density, relative density, hardness and compressive strength were achieved in the case of Mg-Zn/15% Al<sub>2</sub>O<sub>3</sub> at sintering temperature of 300 °C as compared to pure Mg and Mg-Zn alloys in 550 °C.

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